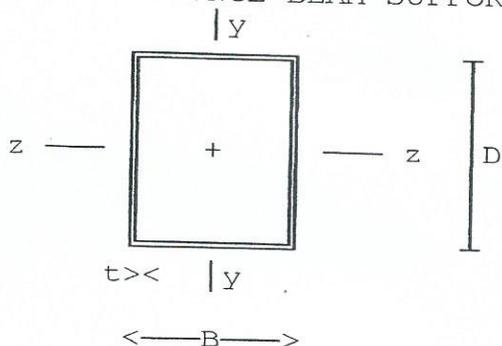


Location: LOUNGE BEAM SUPPORT POST

Office:



RHS Column

Calculations in accordance
 with DESIGN IN SHS to BS449
 published by BSC Tubes Division.

Maximum design BM about axis zz	$M_{zz}' = 3.03$ kNm
Maximum design SF in y direction	$V' = 0$ kN
Design load (comp. positive)	$F' = 61$ kN
Length of member	$L = 2.7$ m
Design BM about yy axis	$M_{yy}' = 3.03$ kNm

Steel section properties

100 x 100 x 10 SHS - Hot finished.

Properties (cm): $A = 34.9$ $r_y = 3.64$ $Z_x = 92.4$ $S_x = 116$ $I_x = 462$ $J = 761$ $C = 133$
 Grade of steel 43

Slenderness ratios

Effective length about yy axis	$l_{yy} = 2700$ mm
Effective length about zz axis	$l_{zz} = 2700$ mm
Slenderness ratio about zz	$l'_{rz} = l_{zz} / (r_z * 10) = 2700 / (3.64 * 10) = 74.176$
Slenderness ratio about yy	$l'_{ry} = l_{yy} / (r_y * 10) = 2700 / (3.64 * 10) = 74.176$
Greatest slenderness ratio	$l'_{r} = l'_{ry} = 74.176$

Axial compression

Calculated compressive stress	$f_c = F / (A * 100) = 61000 / (34.9 * 100) = 17.479$ N/mm ²
Allowable compressive stress	$p_c = \text{TABLE 17 for } l'_{r} = 74.176, \text{ Grade} = 43 = 117.15$ N/mm ²

Since $f_c \leq p_c$ (17.479 N/mm² \leq 117.15 N/mm²) compressive stress within that given in BS449 Table 17, therefore OK.

Bending and local flange instability

Structural hollow sections in the range produced by BSC Tubes Division are not subject to lateral torsional instability, and therefore the full allowable bending stress can be used irrespective of the length of the RHS member.

However, some RHS, where the compression flange width/thickness parameter $(B/t) / K^{0.5}$ exceeds 19.1 and 16.3 for grades 43 and 50 respectively may suffer local instability before reaching full elastic moment, defined by the extreme fibres reaching yield stress. The following check is in accordance with 'DESIGN IN SHS'.

Allowable bending stress	$p_{bc} = 180$ N/mm ²
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